

Ashok Rajpath, Patna, Bihar - 800 005

Incremental Sheet Forming Process

-----Lecture Notes

By

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Incremental Sheet Forming

Incremental forming is a new technique for deforming sheet metals by the application of step by step incremental feed to the deforming tool.

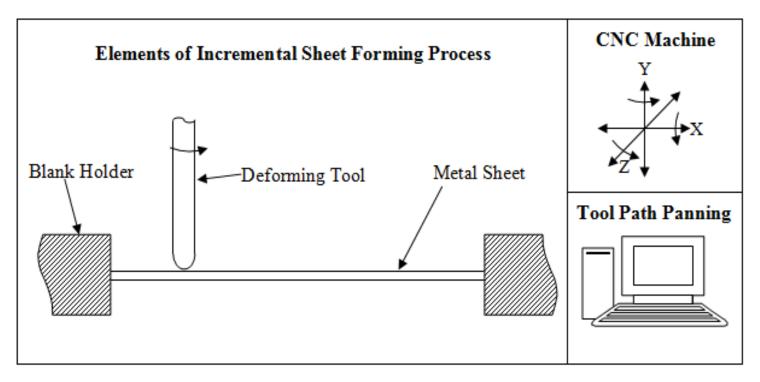


Figure : Incremental Sheet Forming.



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CLASSIFICATION OF ISF

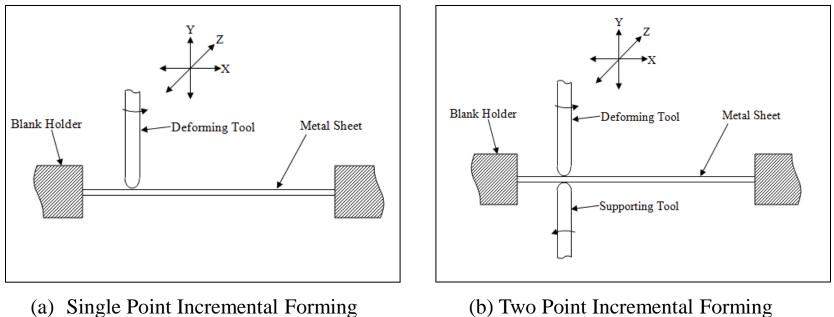
- 1. Conventional Incremental Sheet Forming (CISF)
- 2. Hybrid Incremental Sheet Forming (HISF)

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Conventional Incremental Sheet Forming (CISF)



(SPIF)

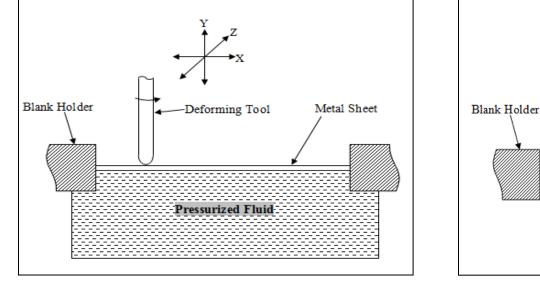
(b) Two Point Incremental Forming (TPIF).

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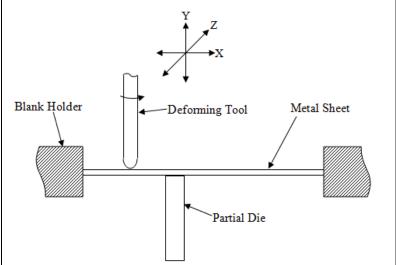


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Hybrid Incremental Sheet Forming (HISF)



(a) Incremental Sheet Hydro-Forming (ISHF).



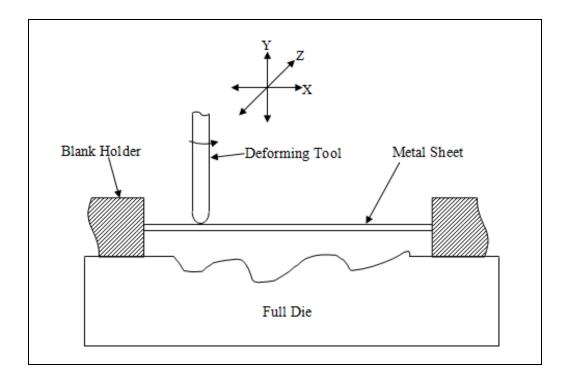
(b) Two Point Incremental Forming with Partial Die (TPIFPD)

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(c) Two Point Incremental Forming with Full Die (TPIFFD).



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ADVANTAGES OF ISF

- Direct forming of usable parts from CAD data
 - Minimum specialized tooling
- Dieless No positive or negative dies needed
- Flexibility Changes in design sizes accommodated easily and quickly
- Formability better
 - Benefit of small plastic zones and incremental nature.
 - Easier to deform low formability sheet.
- Conventional CNC milling/lathe can be used.
- Making of large sized parts possible
 - Forces do not increase because contact zone/step size remain small.
- Operation quiet and noise free relatively.



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DISADVANTAGES OF ISF

- The forming time much higher than competitive processes such as deep drawing.
- Limited to small size batch production.
- The forming of right angles cannot be done in one step, but requires a multi-step process.



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APPLICATIONS OF ISF

- Aerospace Industry: Instrument panel, Body panel, Passenger seat cover etc.
- Automobile: Door inner/outer panel, Hood panel, Engine cover etc.
- High customized products: Denture plate, Ankle support, Metal helmet etc.
- Cellular Telephones
- IC Leadframes
- Electronics
- Healthcare
- Miniature Fasteners
- Hard Disc Drives



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Basic Terminologies in ISF

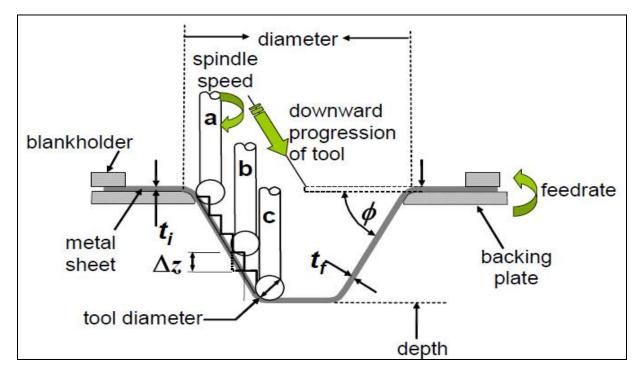


Figure : SPIF Terminology as seen in deformed part (Ham and Jeswiet, Forming Limit Curves in Single Point Incremental Forming 2007).



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Sheet Thinning

1. Thinning in ISF depends on the wall angle α and is given by the sine law $t_1 = t_0 \sin (90^\circ - \alpha)$

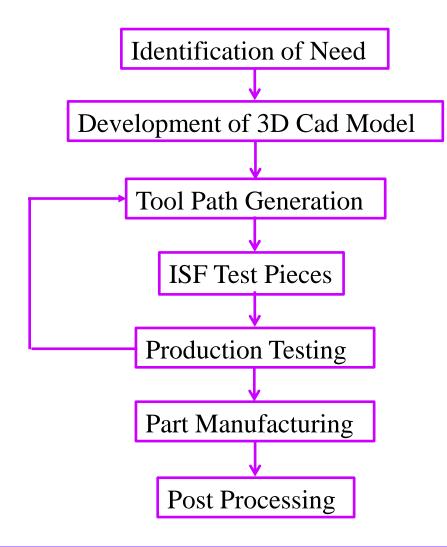


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Development of Single Point Incremental Forming Machine



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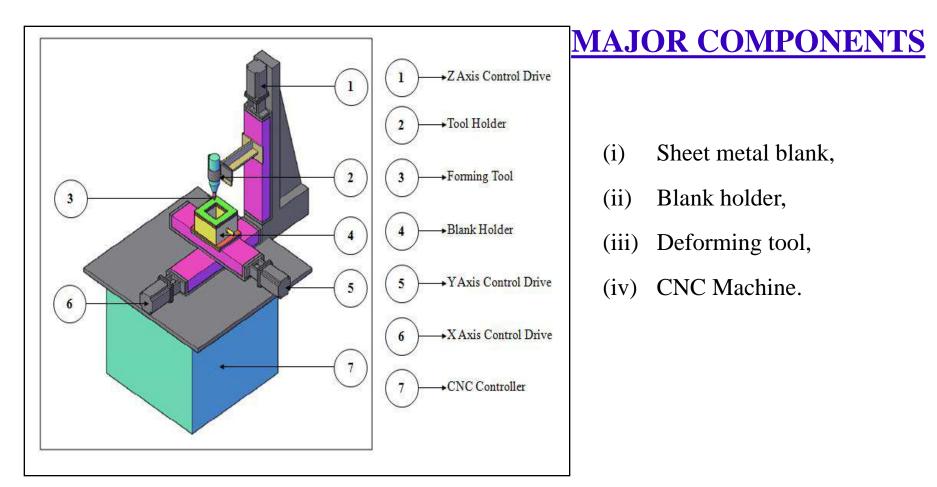


FORMING METHODOLOGY



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INCREMENTAL SHEET FORMING (ISF)





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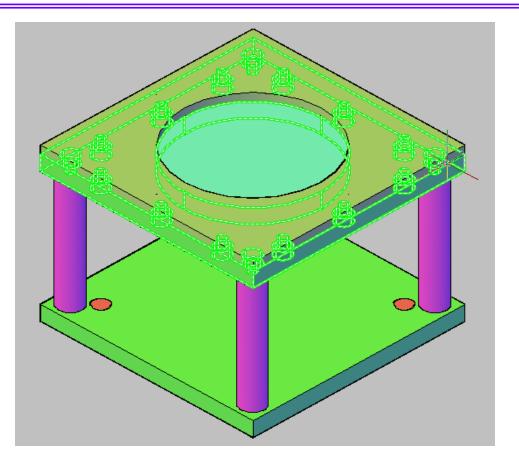


Figure : Blank and Blank holding Arrangement



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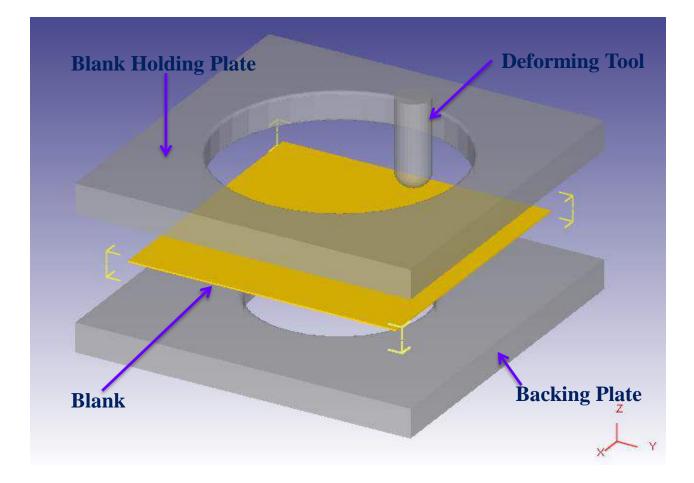


Figure: Exploded view of the Blank and Blank holding Arrangement.

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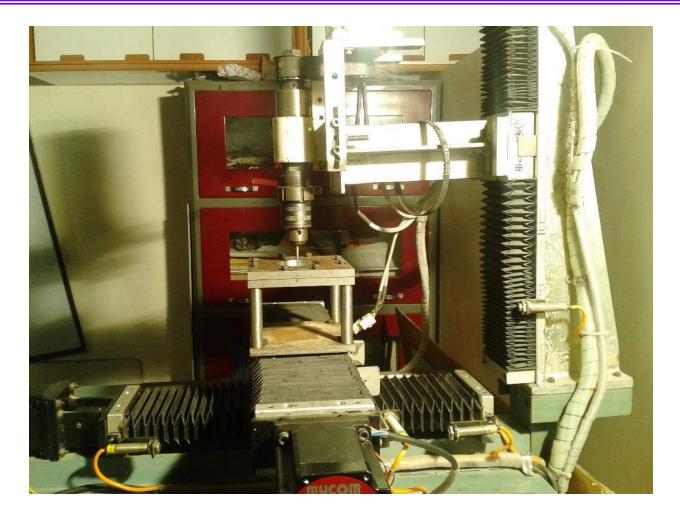


Figure: Single Point Incremental Forming Machine.

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FORMING TOOLS



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18 / 39



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Other Blank Size = (80mm*80mm*0.2mm) Circle Diameter & Pyramid edge= 40 mm, Angle = 45

Figure: Product formed by Dieless Forming Machine

[Top Row : All Aluminum [AL1080A] and Bottom Row from left to Right: 1st Brass, 2nd & 3rd Aluminium and 4th CP Titanium-1].

19 / 39

Titanium Blank Size = (80 mm * 80 mm * 0.4 mm)

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Development of Incremental Sheet Hydroforming Machine



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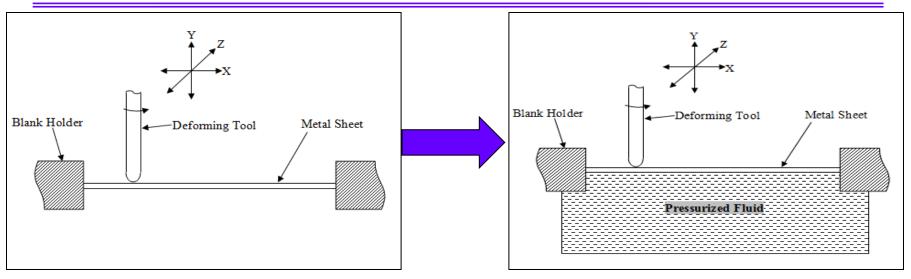


Fig : Incremental Sheet Forming

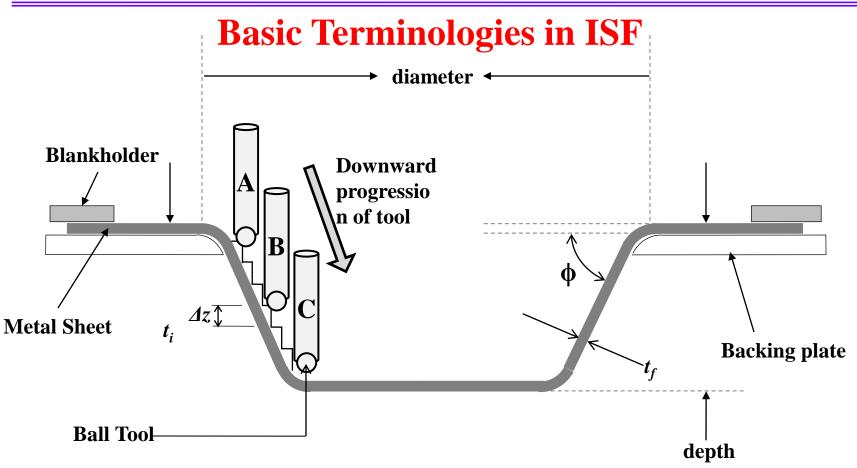
- Strain Distribution : Normal
- Maximum Forming Angle : 67° 69°
- Geometrical inaccuracies
- Crack formation

Fig : Incremental Sheet Hydro Forming

- Strain Distribution : Scope for Improvement
- Maximum Forming Angle : Scope for Improvement
- Geometrical inaccuracies : Scope for Improvement
- Crack formation : less chances of cracks

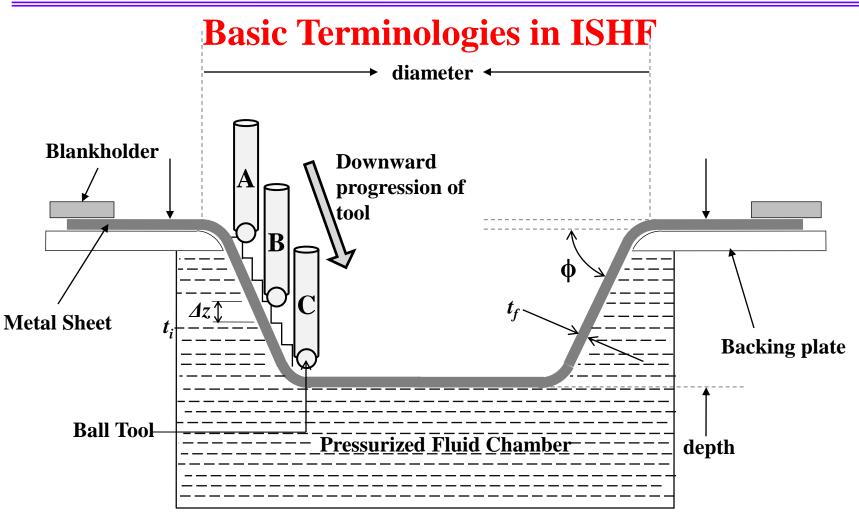


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INCREMENTAL SHEET HYDROFORMING (ISHF)

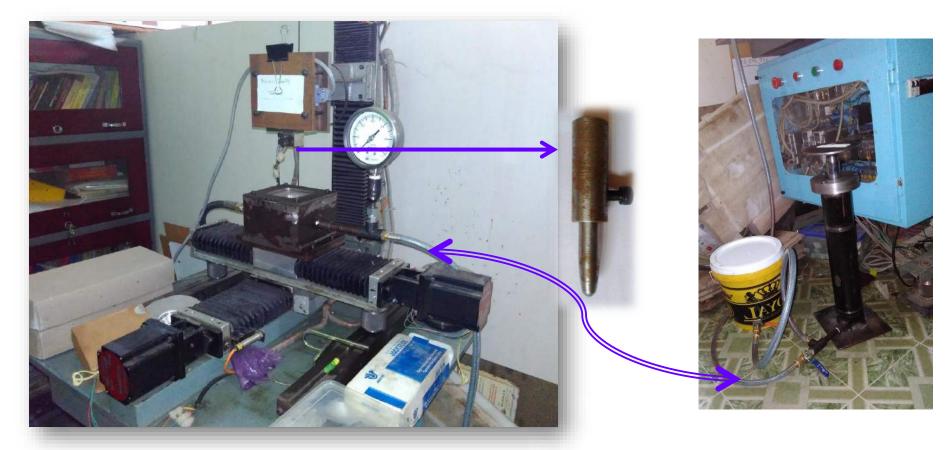


Fig.: Incremental Sheet Hydroforming Machine [Final Modification]

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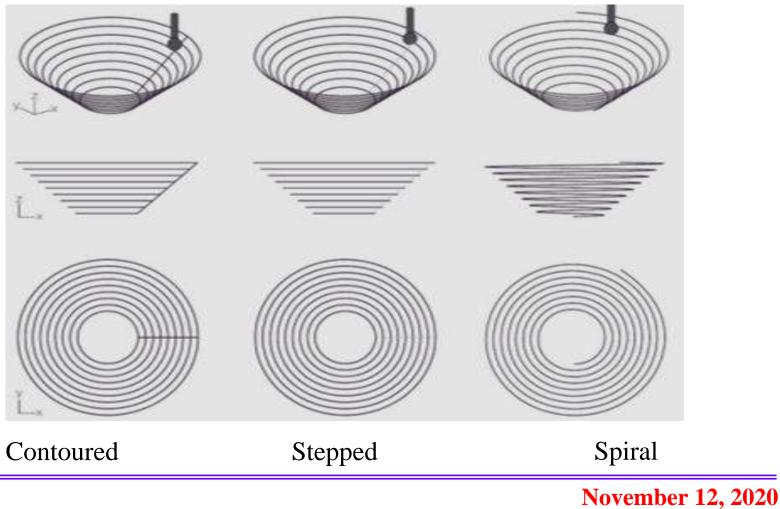


Fig.: FINAL Version of Hydraulic Cylinder



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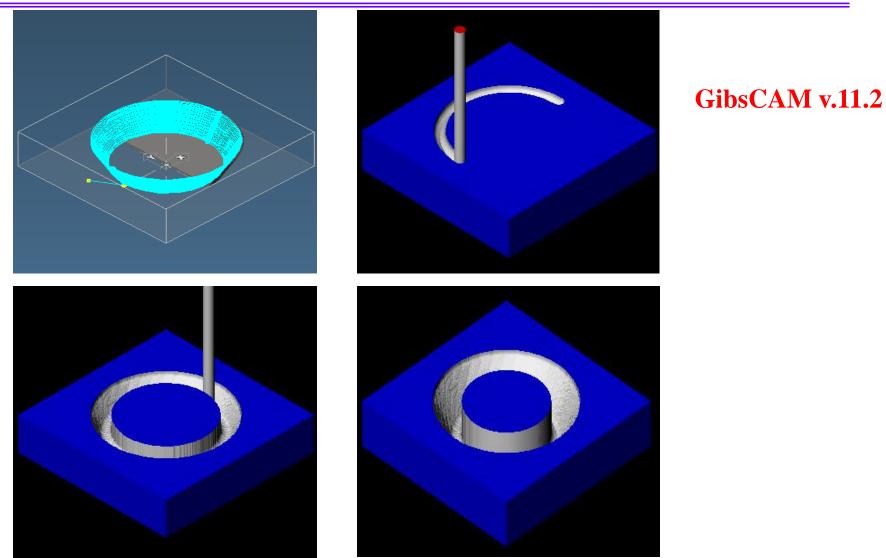
PLANNING FOR TOOL PATH



26 / 39



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Wall Angle (60°), Step Size 0.5

G90 G0 G44 X-17.6155 Y0 Z0 H0 M8 G0 Z1. G1 Z0 F500.0 Y-0.0003 F1000.0 G3 X17.4914 Y0.0001 Z-0.217 I17.5534 J0.0003 X-17.3673 Y0 Z-0.434 I-17.4293 J-0.0001 X17.2432 Z-0.6511 I17.3052 J0 X-17.119 Z-0.8681 I-17.1811 J0 X16.9949 Y0.0001 Z-1.0851 I17.0569 J0 X-16.8708 Y0 Z-1.3021 I-16.9328 J-0.0001 X16.7467 Z-1.5191 I16.8087 J0 X-16.6226 Z-1.7362 I-16.6846 J0 X16.4985 Y0.0001 Z-1.9532 I16.5605 J0 X-16.3744 Y0 Z-2.1702 I-16.4364 J-0.0001 X16.2503 Z-2.3872 I16.3123 J0 X-16.1262 Z-2.6042 I-16.1882 J0 X16.0021 Z-2.8213 I16.0641 J0 X-15.878 Z-3.0383 I-15.94 J0 X15.7539 Z-3.2553 I15.8159 J0 X-15.6298 Z-3.4723 I-15.6918 J0 X15.5057 Y0.0007 Z-3.6893 I15.5677 J0 X-15.3816 Y0 Z-3.9064 I-15.4436 J-0.0007 X15.2575 Z-4.1234 I15.3195 J0 X-15.1334 Z-4.3404 I-15.1954 J0 X15.0092 Z-4.5574 I15.0713 J0 X-14.8851 Z-4.7744 I-14.9471 J0 X14.761 Z-4.9915 I14.823 J0 X-14.6369 Z-5.2085 I-14.6989 J0 X14.5128 Z-5.4255 I14.5748 J0

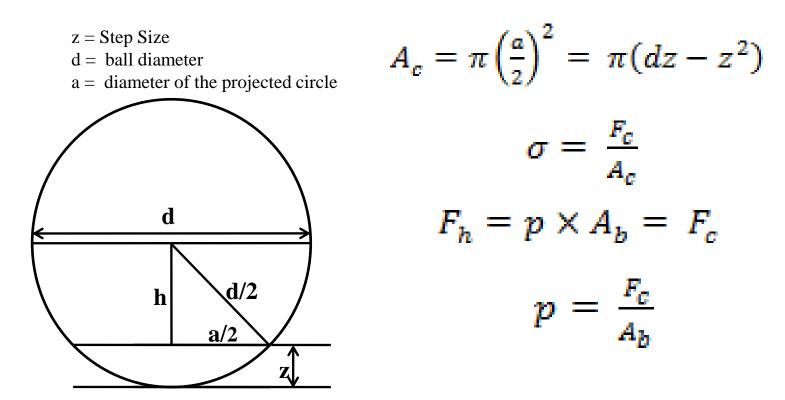
X-14.3887 Z-5.6425 I-14.4507 J0 X14.2646 Z-5.8595 I14.3266 J0 X-14.1405 Z-6.0766 I-14.2025 J0 X14.0164 Z-6.2936 I14.0784 J0 X-13.8923 Z-6.5106 I-13.9543 J0 X13.7682 Z-6.7276 I13.8302 J0 X-13.6441 Z-6.9446 I-13.7061 J0 X13.52 Z-7.1617 I13.582 J0 X-13.3959 Z-7.3787 I-13.4579 J0 X13.2718 Z-7.5957 I13.3338 J0 X-13.1477 Z-7.8127 I-13.2097 J0 X13.0236 Z-8.0297 I13.0856 J0 X-12.8994 Z-8.2468 I-12.9615 J0 X12.7753 Z-8.4638 I12.8373 J0 X-12.6512 Z-8.6808 I-12.7132 J0 X12.5271 Z-8.8978 I12.5891 J0 X-12.403 Z-9.1148 I-12.465 J0 X12.2789 Z-9.3319 I12.3409 J0 X-12.1548 Z-9.5489 I-12.2168 J0 X12.0307 Z-9.7659 I12.0927 J0 X-11.9066 Z-9.9829 I-11.9686 J0 X11.7825 Z-10.1999 I11.8445 J0 X-11.6584 Z-10.417 I-11.7204 J0 X11.5343 Z-10.634 I11.5963 J0 X-11.4102 Z-10.851 I-11.4722 J0 X11.2861 Z-11.068 I11.3481 J0 X-11.162 Z-11.285 I-11.224 J0 X11.0379 Z-11.5021 I11.0999 J0 X-10.9137 Z-11.7191 I-10.9758 J0 X10.7896 Z-11.9361 I10.8516 J0

X-10.6655 Z-12.1531 I-10.7275 J0 X10.5414 Z-12.3701 I10.6034 J0 X-10.4173 Z-12.5872 I-10.4793 J0 X10.2932 Z-12.8042 I10.3552 J0 X-10.1691 Z-13.0212 I-10.2311 J0 X10.045 Z-13.2382 I10.107 J0 X-9.9209 Z-13.4552 I-9.9829 J0 X9.7968 Z-13.6723 I9.8588 J0 X-9.6727 Z-13.8893 I-9.7347 J0 X9.5486 Z-14.1063 I9.6106 J0 X-9.4245 Z-14.3233 I-9.4865 J0 X9.3004 Z-14.5403 I9.3624 J0 X-9.1763 Z-14.7574 I-9.2383 J0 X9.0522 Z-14.9744 I9.1142 J0 X-8.9281 Z-15.1914 I-8.9901 J0 X8.8039 Z-15.4084 I8.866 J0 X-8.6798 Z-15.6254 I-8.7418 J0 X8.5557 Z-15.8425 I8.6177 J0 X-8.4316 Z-16.0595 I-8.4936 J0 X8.3075 Z-16.2765 I8.3695 J0 X-8.1834 Z-16.4935 I-8.2454 J0 X8.0593 Z-16.7105 I8.1213 J0 X-7.9352 Z-16.9276 I-7.9972 J0 X7.8111 Z-17.1446 I7.8731 J0 X-7.687 Z-17.3616 I-7.749 J0 17.687 J0 G0 Z50. G91 G28 X0 Y0 Z0 M30



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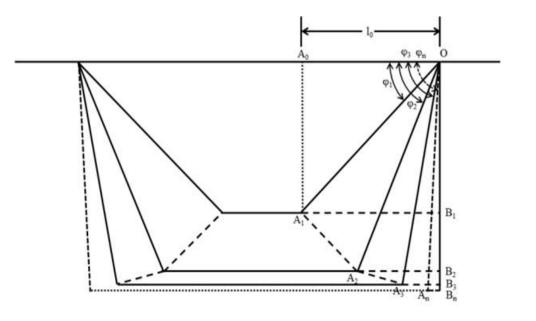
Analysis of Forming Force, Stresses in the contact area and Applied Pressure





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Multi-Stage & Multi-Step Forming Strategy for ISHF to achieve high forming angle



 l_0 = Initial length of sheet under forming l_1 = Length of sheet under forming after first step x_1 = Total increment in X direction in 1st step l_n = Length of sheet under forming after *n* steps X_n = Total increment in X direction in *n*th step Z_n = Total increment in Z direction in *n*th step From the right angled triangle A_0OA_1 $l_1 = \frac{l_0}{cos\phi_1}$ $X_1 = l_1cos\phi_1$

 $Z_1 = l_1 sin\phi_1$

Figure : Multi-Stage & Multi-Step Forming Strategy



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Table : Multi-Stage & Multi-Step Forming Strategy

Step No.(n)	Forming Angle (ϕ_n)	Forming Length (l_n)	X_n	Z_n	ΔZ_n
1	$\phi_1 = \frac{\pi}{4}$	$l_1 = \frac{l_0}{\cos\phi_1}$	$x_1 = l_1 cos\phi_1$	$z_1 = l_1 sin\phi_1$	$\Delta Z_1 = t_0$
2	$\phi_2 = \frac{3\pi}{8}$	$l_2 = \frac{l_1}{\cos(\phi_2 - \phi_1)}$	$x_2 = l_2 cos\phi_2$	$z_2 = l_2 sin\phi_2$	$\Delta Z_2 = \Delta Z_1/2$
3	$\phi_3 = \frac{7\pi}{16}$	$l_3 = \frac{l_2}{\cos(\phi_3 - \phi_2)}$	$x_3 = l_3 cos\phi_3$	$z_3 = l_3 sin\phi_3$	$\Delta Z_3 = \Delta Z_2/2$
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0.05		0.5	•		
	•	•			•
n	$\phi_n = \frac{\pi}{2}(1-\frac{1}{2^n})$	$l_n = \frac{l_{n-1}}{\cos(\phi_n - \phi_{(n-1)})}$	$x_n = l_n \cos\phi_n$	$z_n = l_n sin\phi_n$	$\Delta Z_n = \Delta Z_{n-1}/2$

The analytical modeling to predict the sheet thinning in final product.



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Table : Experimental Details : Multi-Stage & Multi-Step Forming Strategy [Experiment No. 1]

Step No.(<i>n</i>)	Forming Angle (ϕ_n)	Forming Length (l_n)	X_n	Z_n	ΔZ_n
1	45 ^o	$l_1 = 14.14mm$	$x_1 = 10.00mm$	$z_1 = 10.00mm$	0.5mm
2	67.50°	$l_2 = 15.31mm$	$x_2 = 5.86mm$	$z_2 = 14.14mm$	0.25mm
3	78.75 ^o	$l_3 = 15.61mm$	$x_3 = 3.05mm$	$z_3 = 15.31mm$	0.125mm

Table : Experimental Details : Multi-Stage & Multi-Step Forming Strategy [Experiment No. 2]

Step No.(<i>n</i>)	Forming Angle (ϕ_n)	Forming Length (l_n)	X_n	Z_n	ΔZ_n
1	45°	$l_1 = 21.21mm$	$x_1 = 15.00mm$	$z_1 = 15.00mm$	0.5mm
2	67.50°	$l_2 = 22.96mm$	$x_2 = 8.79mm$	$z_2 = 21.21mm$	0.25mm
3	78.75°	$l_3 = 23.43mm$	$x_3 = 4.57mm$	$z_3 = 22.98mm$	0.125mm



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Figure : Crack Formation in Multi-Stage & Multi-Step Forming Strategy for first experiment



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Figure : Crack Formation in Multi-Stage & Multi-Step Forming Strategy for second experiment



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Scope for Improvement in Multi-Stage & Multi-Step Forming Strategy

Thickness = 0.5 mmAngle = 90° Blank Diameter : 125 mm



Figure : Failure in Circular Component at angle 90°



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Analytical Model for Modified MSMS Forming Strategy

$$t_{Wall} = \frac{t_o}{2} \left(1 - \frac{l}{2R} \right) \tag{1}$$

$$t_{Bottom} = \frac{t_o}{2} \left[\frac{\left(1 - \frac{5l}{6R}\right)}{\left(1 - \frac{l}{3R}\right)} \right]$$
(2)

- $t_o =$ initial sheet thickness
- R = radius of circular section
- l =depth of circular section
- t_{Wall} = final thickness at depth *l* in vertical portion of sheet at corner
- t_{Bottom} = final thickness *l* in horizontal portion of sheet at corner



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Experimental Results



$$\Delta Z_h = \frac{\Delta Z_o}{2} \left(1 - \frac{h}{2R} \right)$$

$$p_h = \frac{p_o}{2} \left[\frac{\left(1 - \frac{5h}{6R}\right)}{\left(1 - \frac{h}{3R}\right)} \right]$$

Figure : Final product after implementation Modified MSMS Forming Strategy



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Multi-Feature Products using ISHF



Figure : Multi- Feature Case 1



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Multi-Feature Products using ISHF



Figure : Multi- Feature Case 2

Stretch Forming

Stretch Forming

Sheet metal is stretched and simultaneously bent to achieve shape change

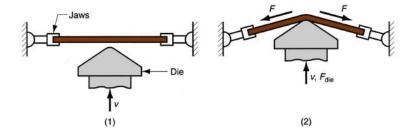


Figure: Stretch forming: (1) start of process; (2) form die is pressed into the work with force Fdie, causing it to be stretched and bent over the form. F = stretching force Spinning

Spinning

Metal forming process in which an axially symmetric part is gradually shaped over a rotating mandrel using a rounded tool or roller

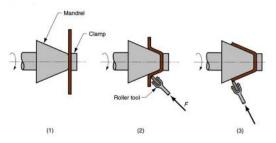


Figure: Conventional spinning: (1) setup at start of process; (2) during spinning; and (3) completion of process